

# The Time-of-Flight Detector for the ALICE experiment

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Subject of this talk:

“A quick review of 2 years’ R&D of the multigap RPC”

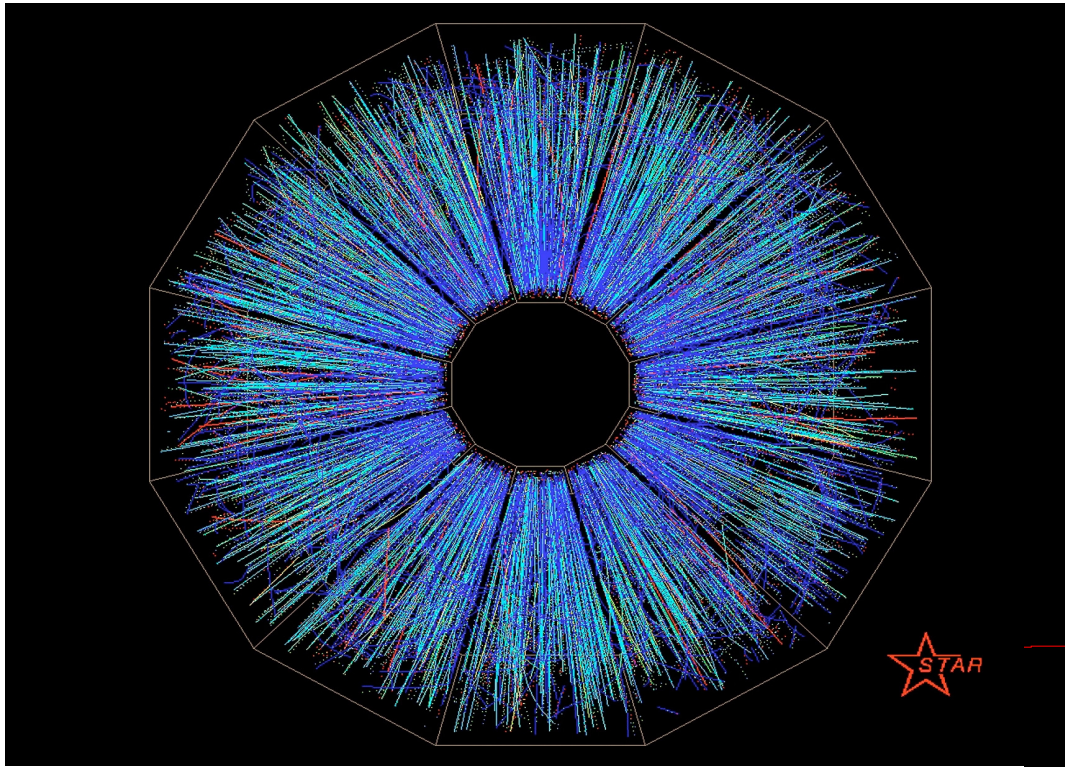
Question: What is needed for the ALICE TOF detector?

Answer:

- (1) Highly segmented detector (160,000 channels)
- (2) Large area 150 m<sup>2</sup> (i.e. low cost)
- (3) Time resolution ~100 ps

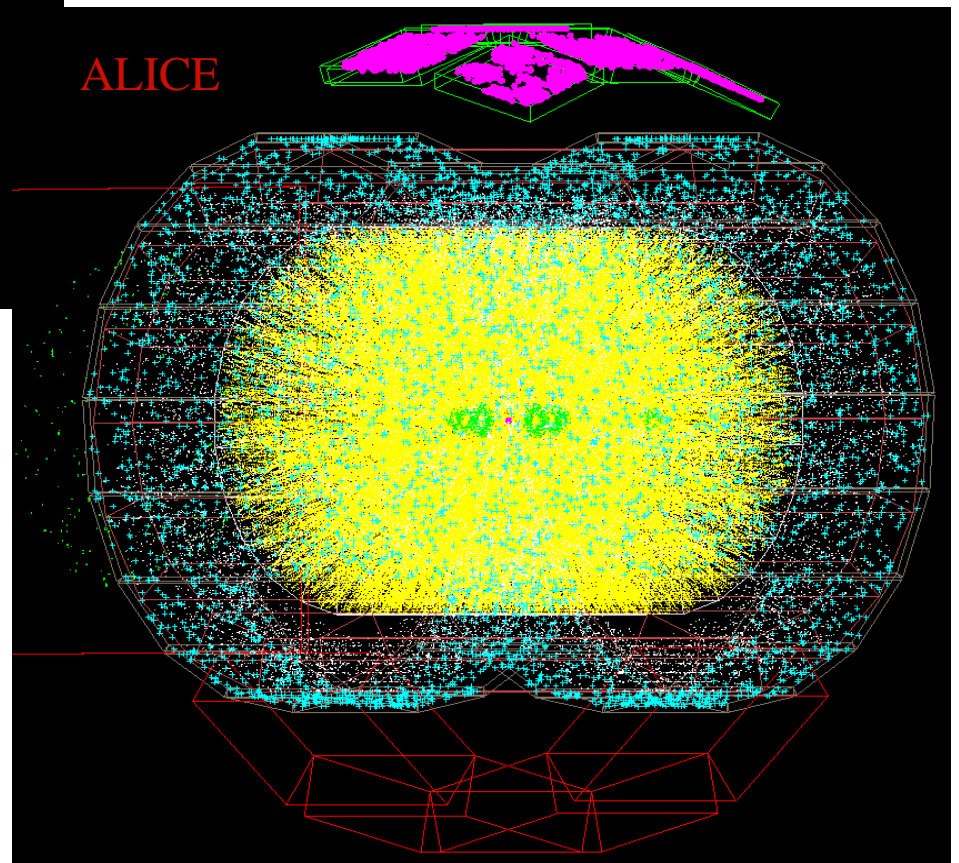


The Multigap Resistive Plate Chamber



Question: How do we make sense of this?

Answer: Identify each particle - or at least as many as possible.





Hits in inner  
tracker

TPC hits

The red hits/track  
corresponds to a  
single particle  
( $\pi$  in this case)

Hits in TOF array

TOF with very high granularity needed!

## ALICE TOF

covers 150 m<sup>2</sup>

consists of 160,000 readout channels.

Each pad is 2.5 x 3.5 cm<sup>2</sup>.

Occupancy ~ 12% (if 8,000 particles produced per unit of rapidity)

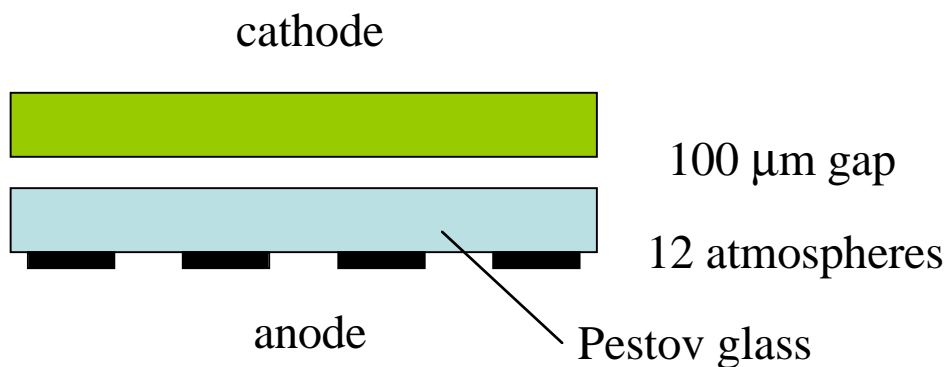
‘Standard’ TOF system built of scintillators plus phototubes would cost  
~ 80 MCHF

Gaseous detectors route to large area detectors at affordable price.

## Two gaseous detectors considered for ALICE

### Pestov counters

Glass electrode and metal electrode



Excellent time resolution  $\sim 50$  ps

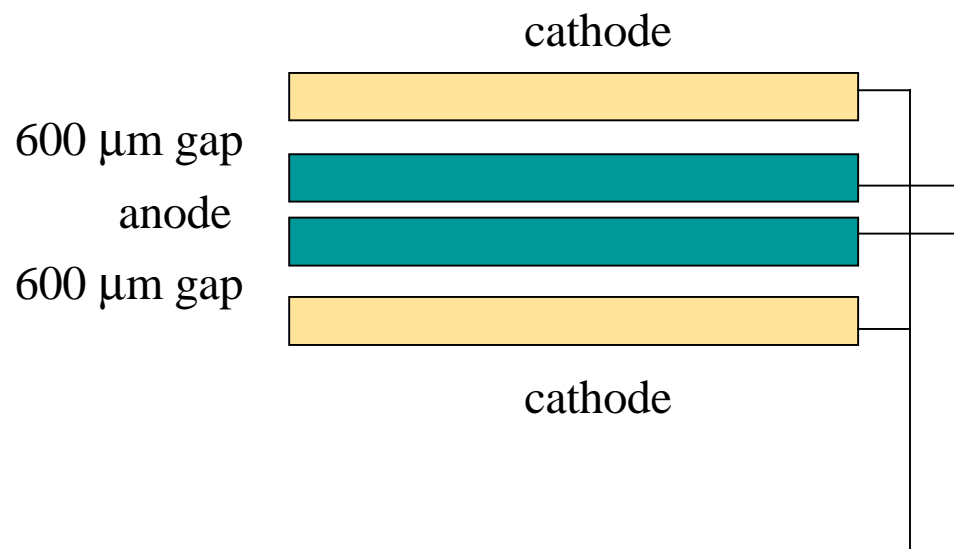
But long tail of late events

Mechanical constraints (due to high pressure)

Non-commercial glass

### Double gap PPC

Both electrodes metallic



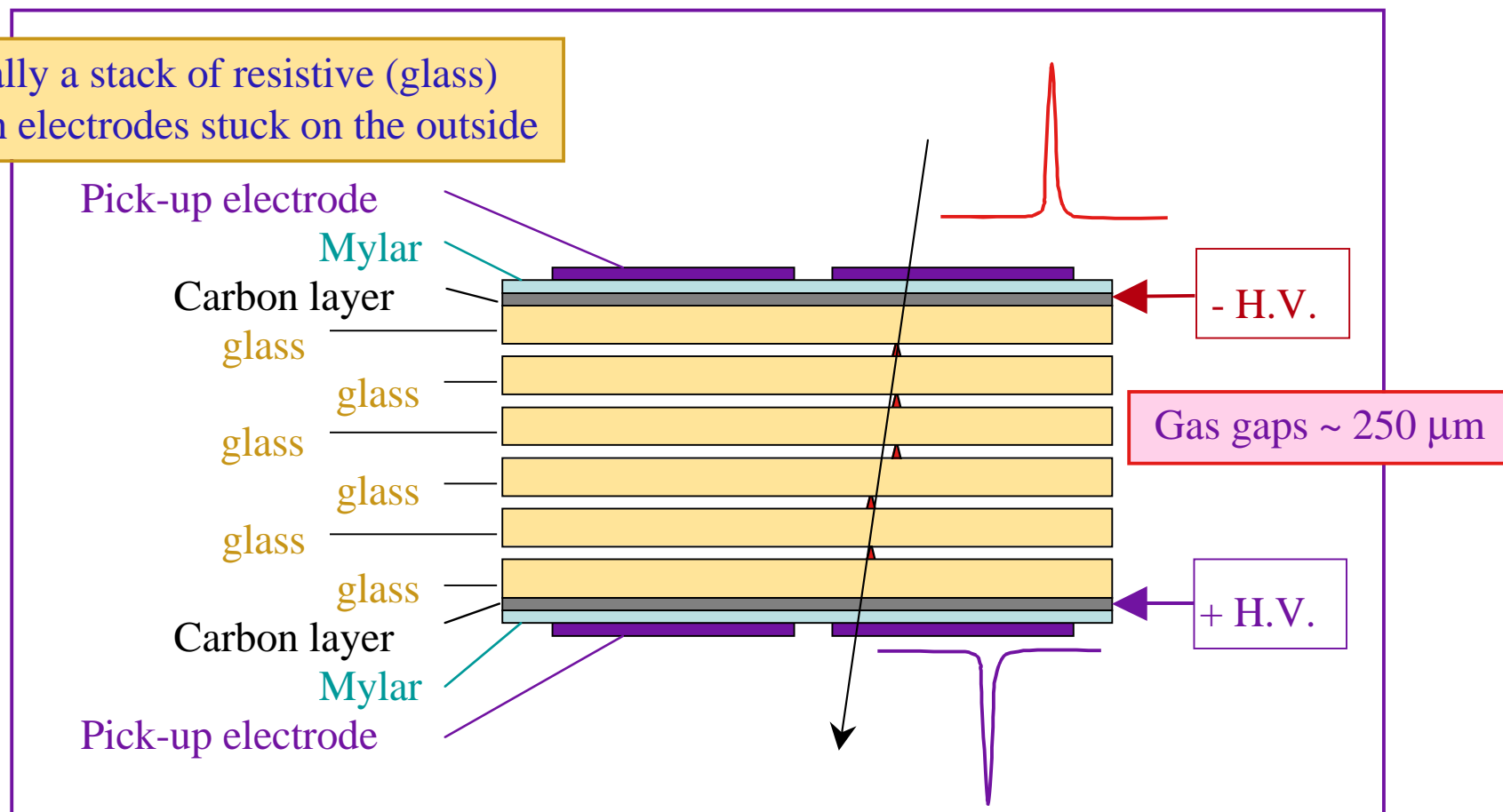
Marginal time resolution  $\sim 250$  ps

Small signal (to keep sparks at low probability)

Difficult to build

## The MULTIGAP Resistive Plate Chamber

Essentially a stack of resistive (glass) plates with electrodes stuck on the outside



Note 1: internal glass plates electrically floating - take and keep correct voltage by electrostatics and flow of electrons and ions produced in gas avalanches

Note 2: resistive plates transparent to fast signals - induced signals on external electrodes is sum of signals from all gaps

# History

November 1998

First tests of MRPCs for ALICE TOF

April 1999

INFN Bologna joins ALICE  
lead group for TOF based on MRPCs

January 2000

ALICE TOF TDR submitted

Period of intense R&D - what problems - what solutions?

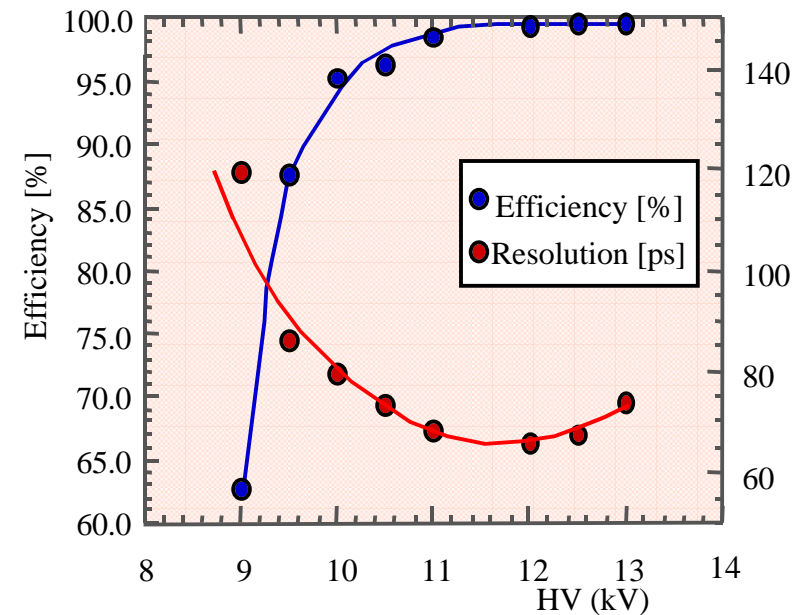
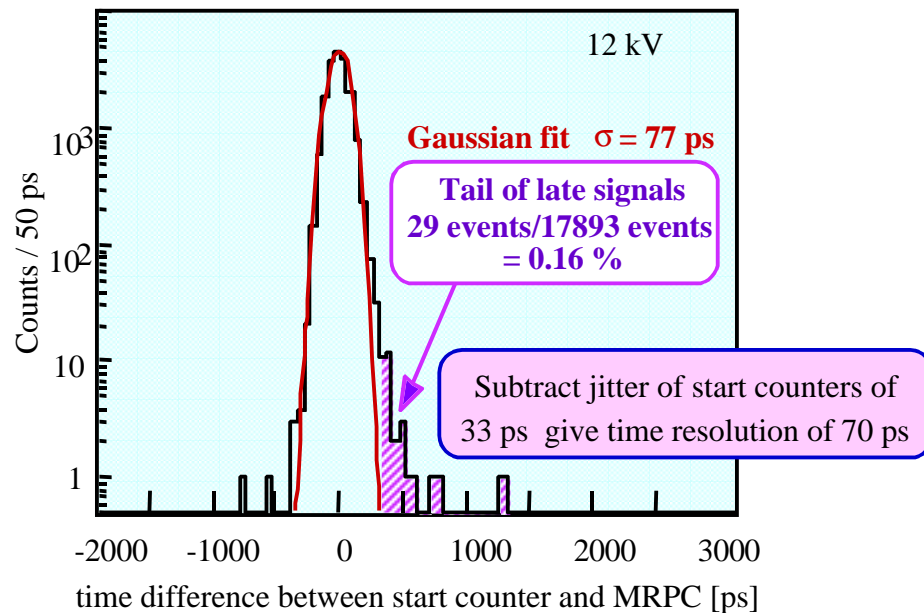
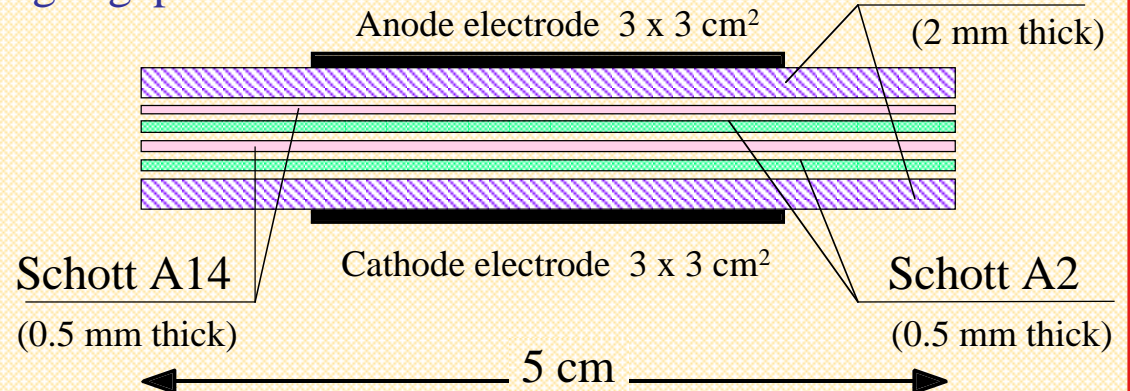


Starting point  
Spring 1999

Single cell  $3 \times 3 \text{ cm}^2$  active area

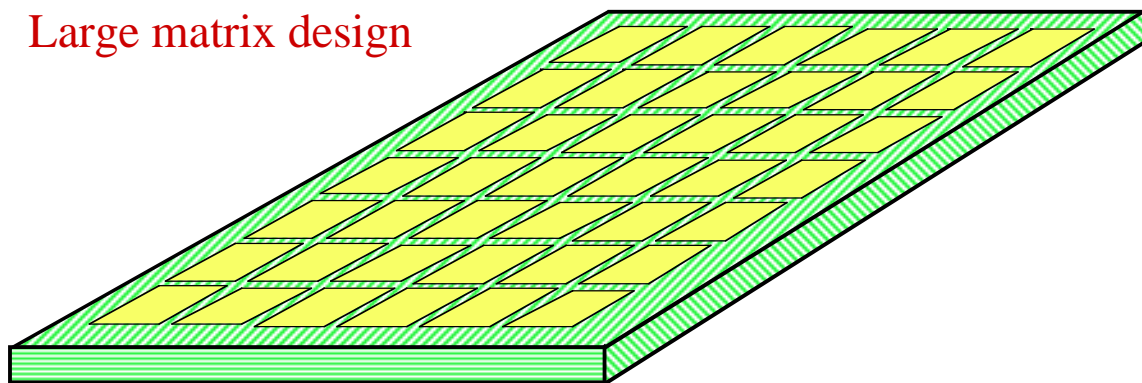
Question:  
Can we build big  
device with similar  
performance to small  
single cells?

5 gas gaps of 220 micron



1999 tests: Two 'large'  
designs tested - large  
matrix and strip

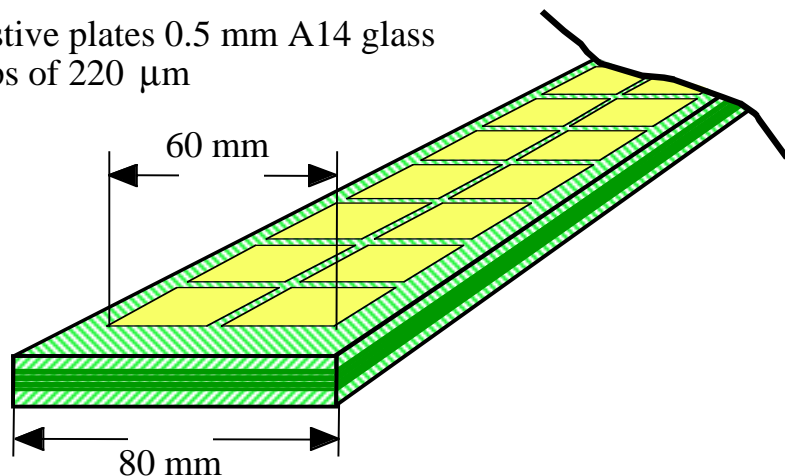
Large matrix design



Various sizes with various materials tested

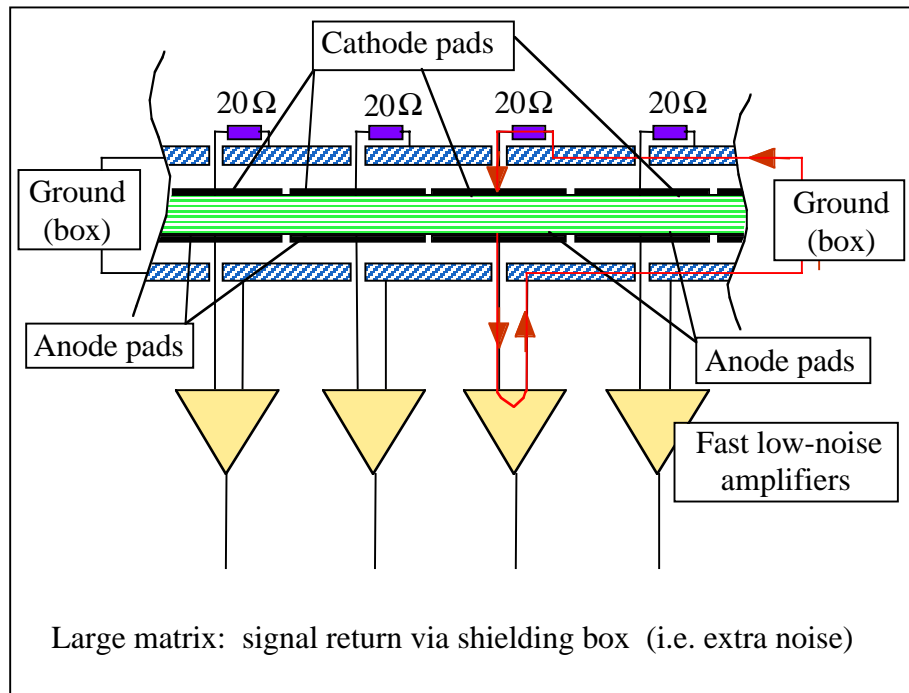
### Strip design of MRPC

Resistive plates 0.5 mm A14 glass  
5 gaps of 220  $\mu\text{m}$



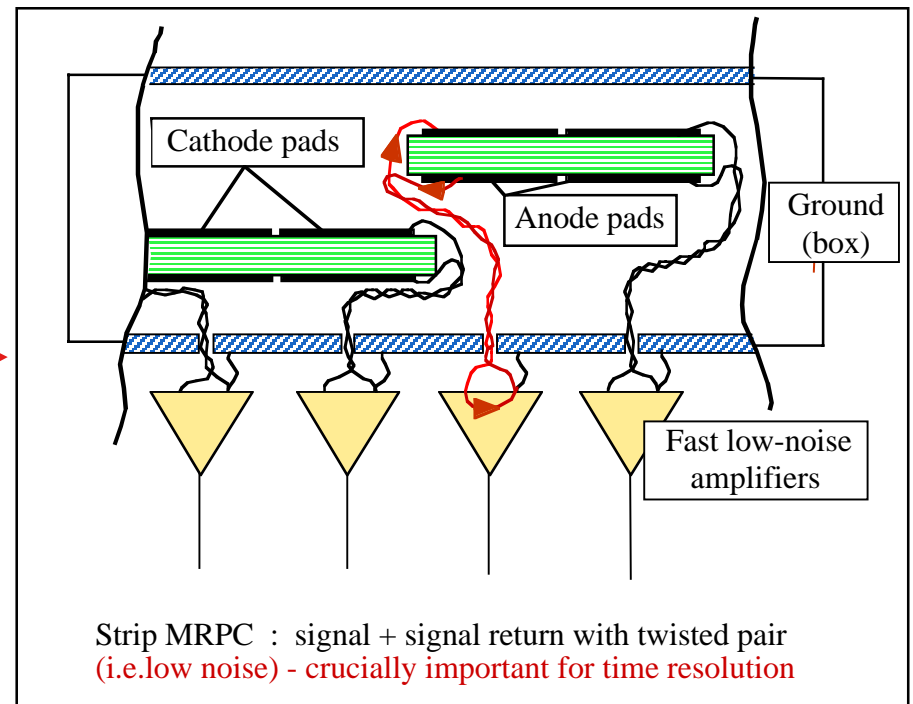
Allows tilting of strips so detector  
normal to incoming particles - this suits  
ALICE geometry better and **also allows**  
differential read-out of detector

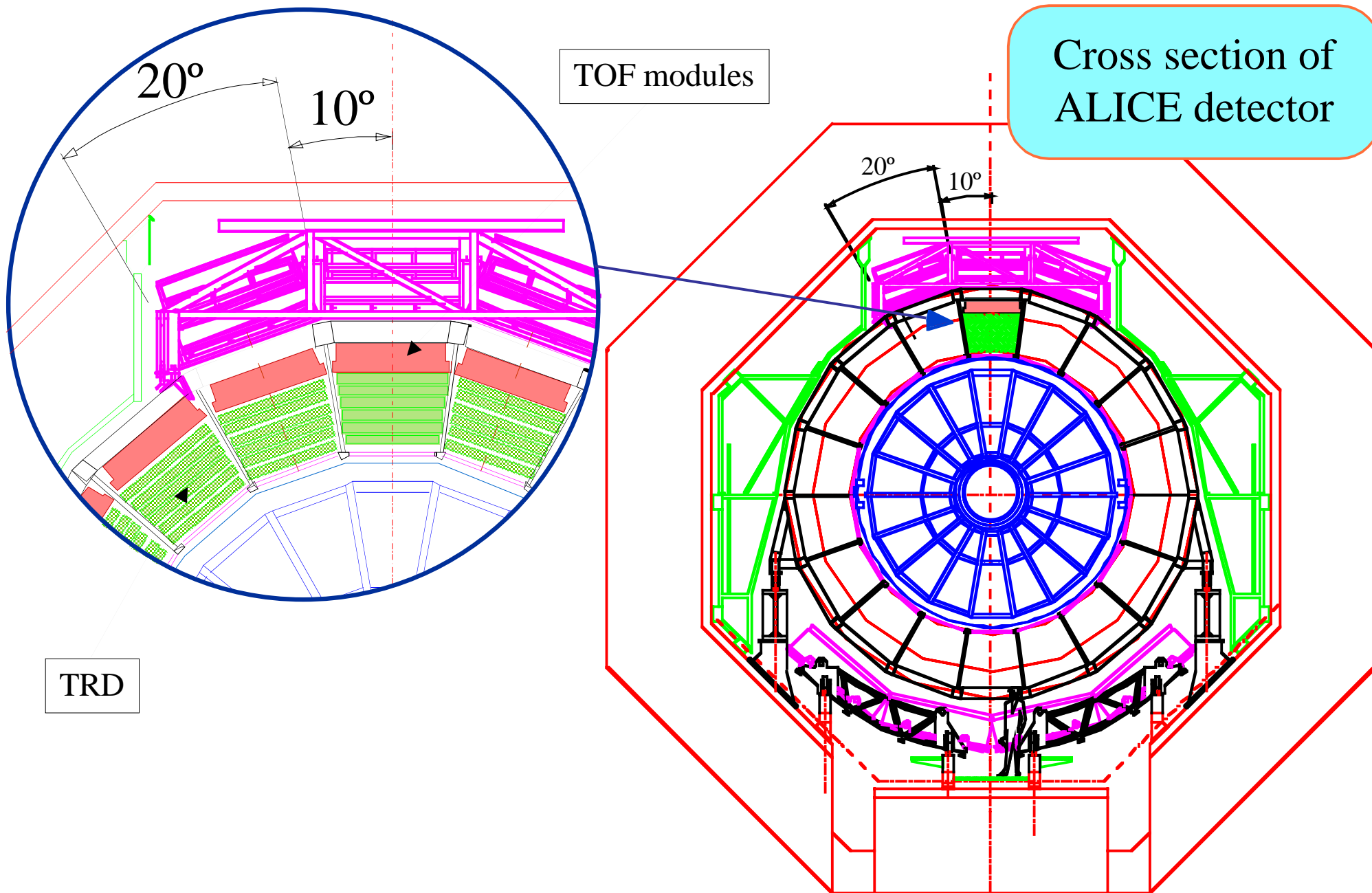
See next transparency

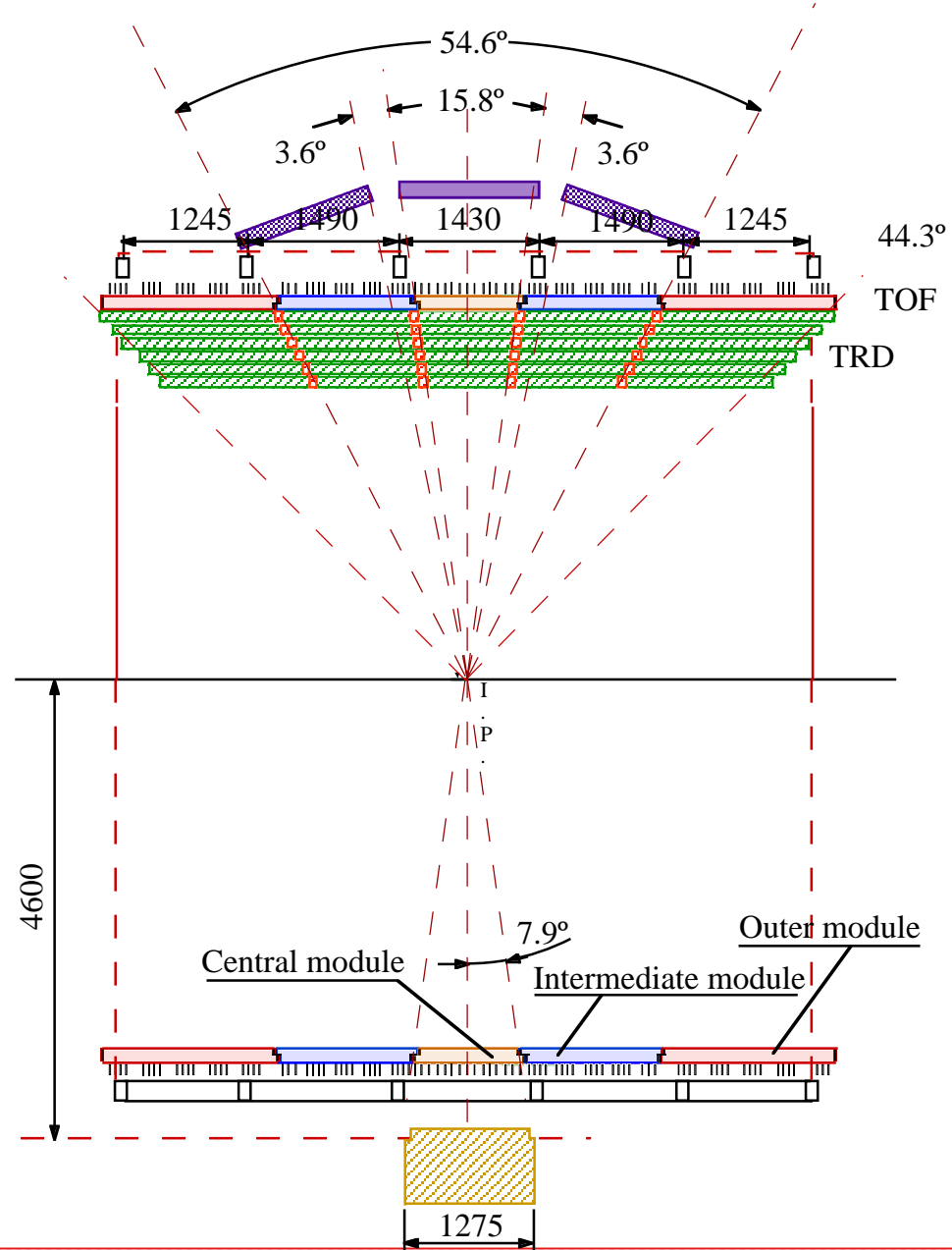


Signal created between anode and cathode - but amplifiers measure anode signal w.r.t. ground

Problems related to noise and stability disappeared with this implementation

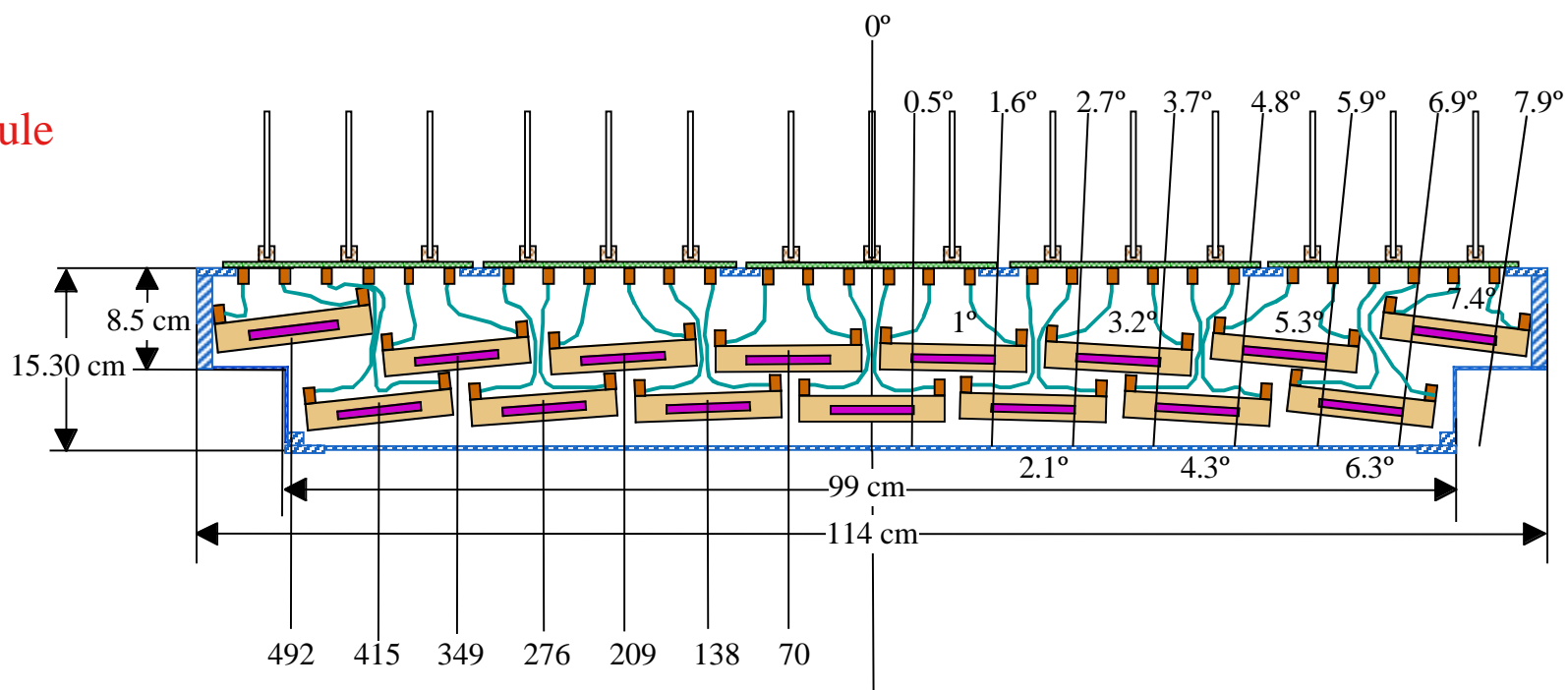




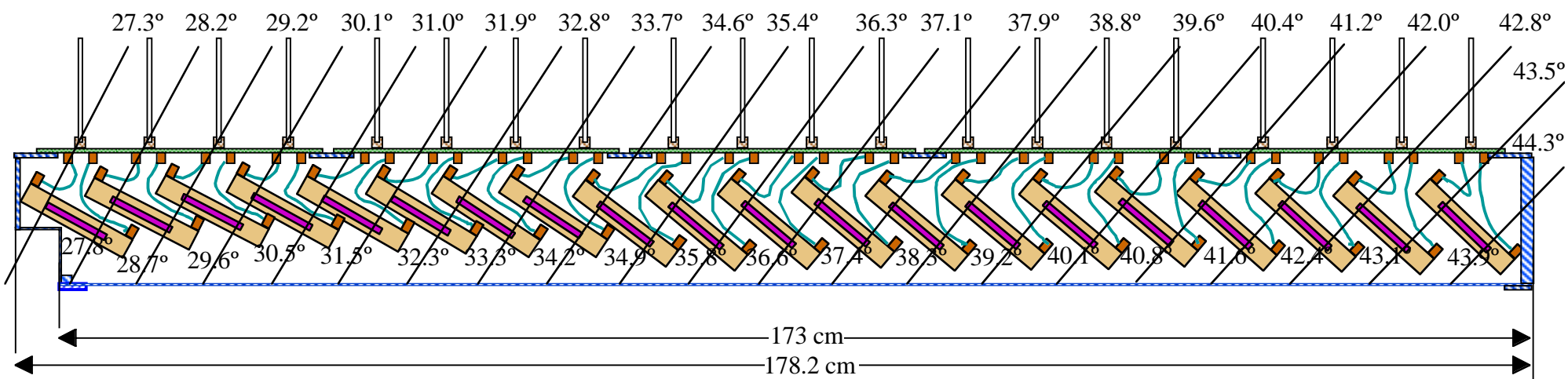




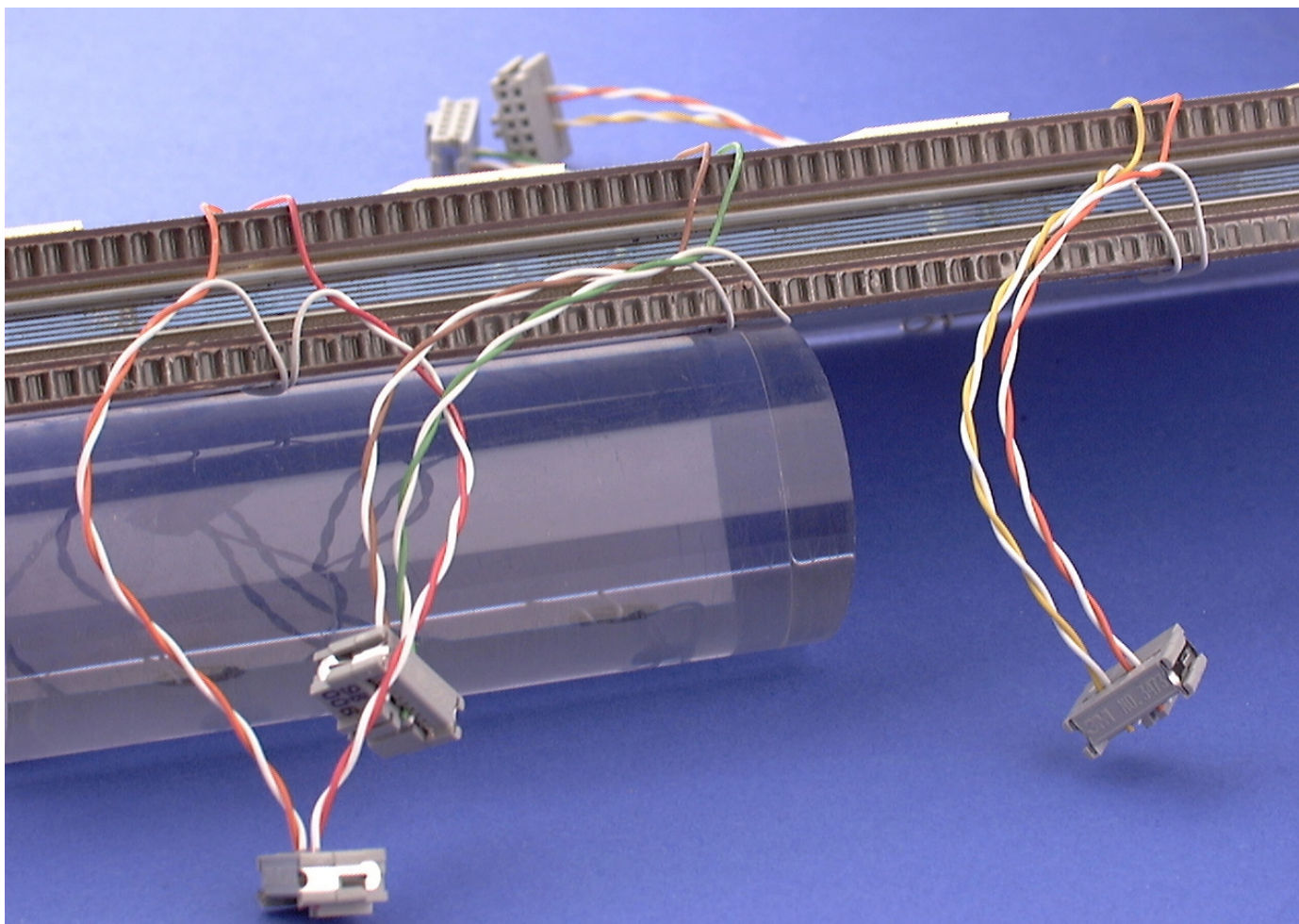
## Central module



## Outer module

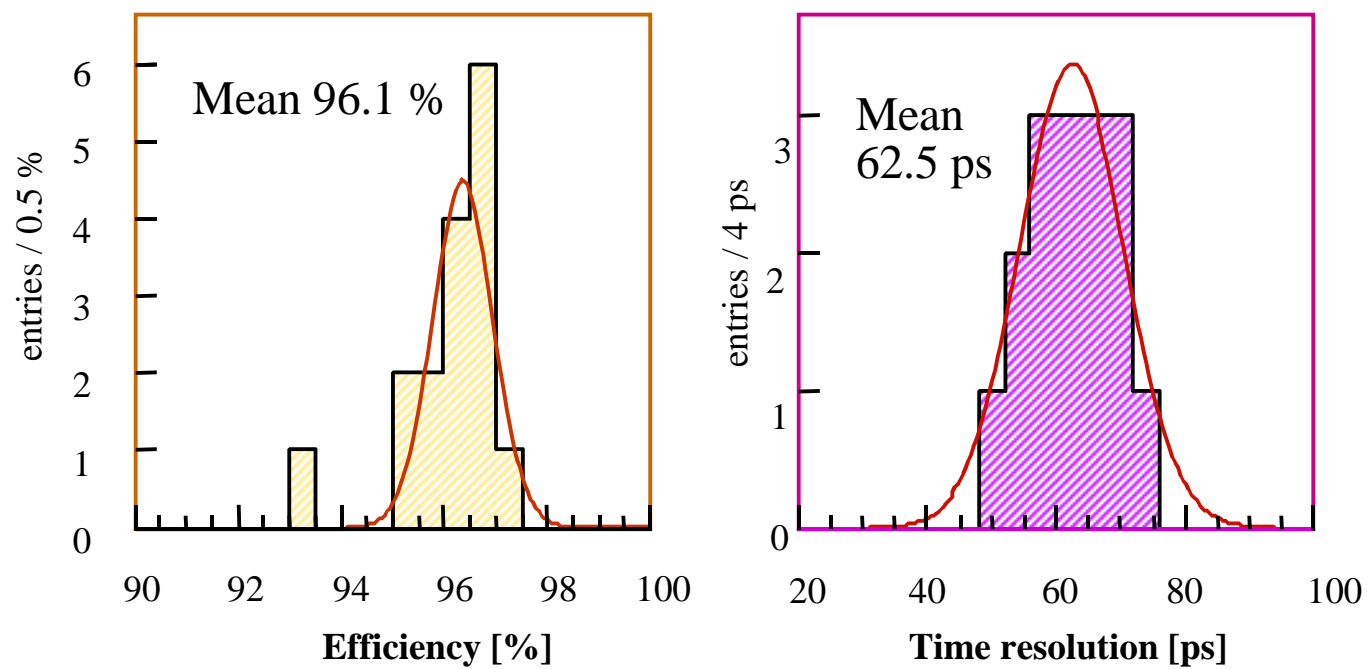


November 1999  
Built and tested 16 pad strip active area  $24 \times 6 \text{ cm}^2$



16 pad strip works just fine!

8x2 cell strip detector 12.5 kV

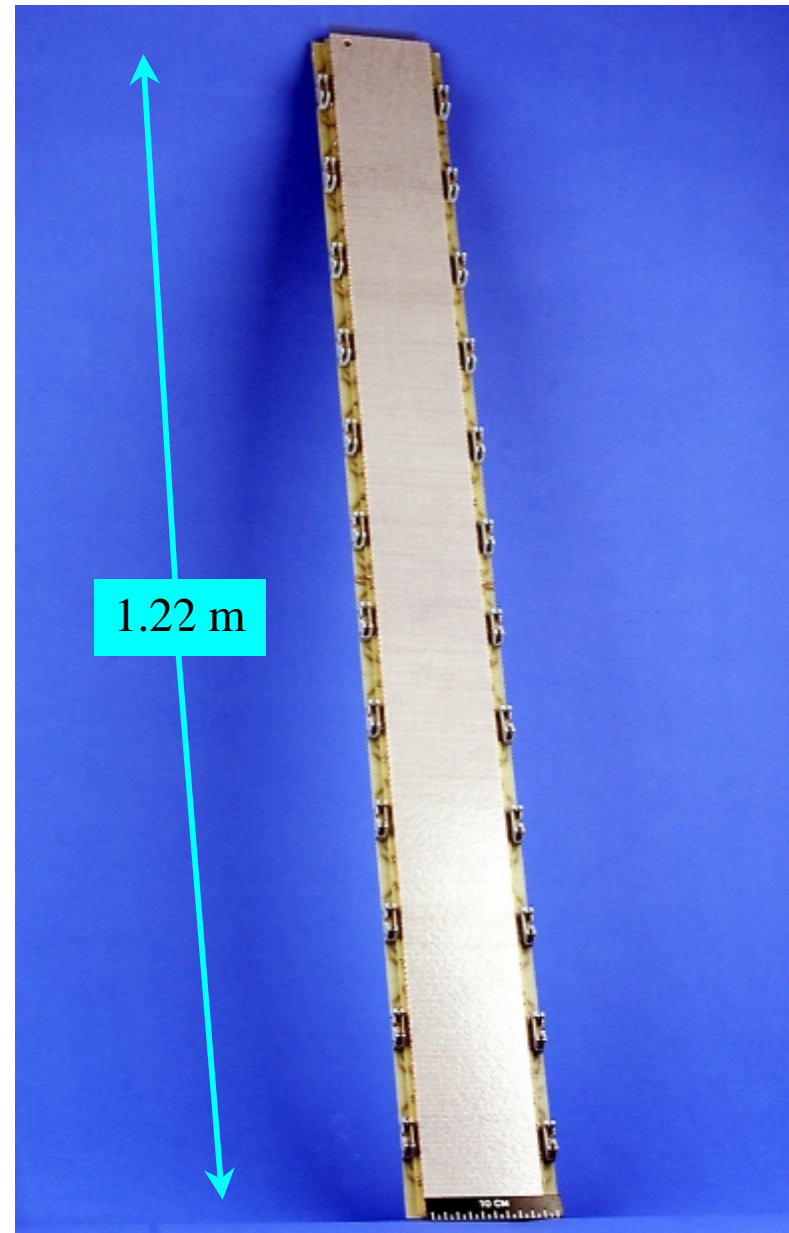


Spring 2000

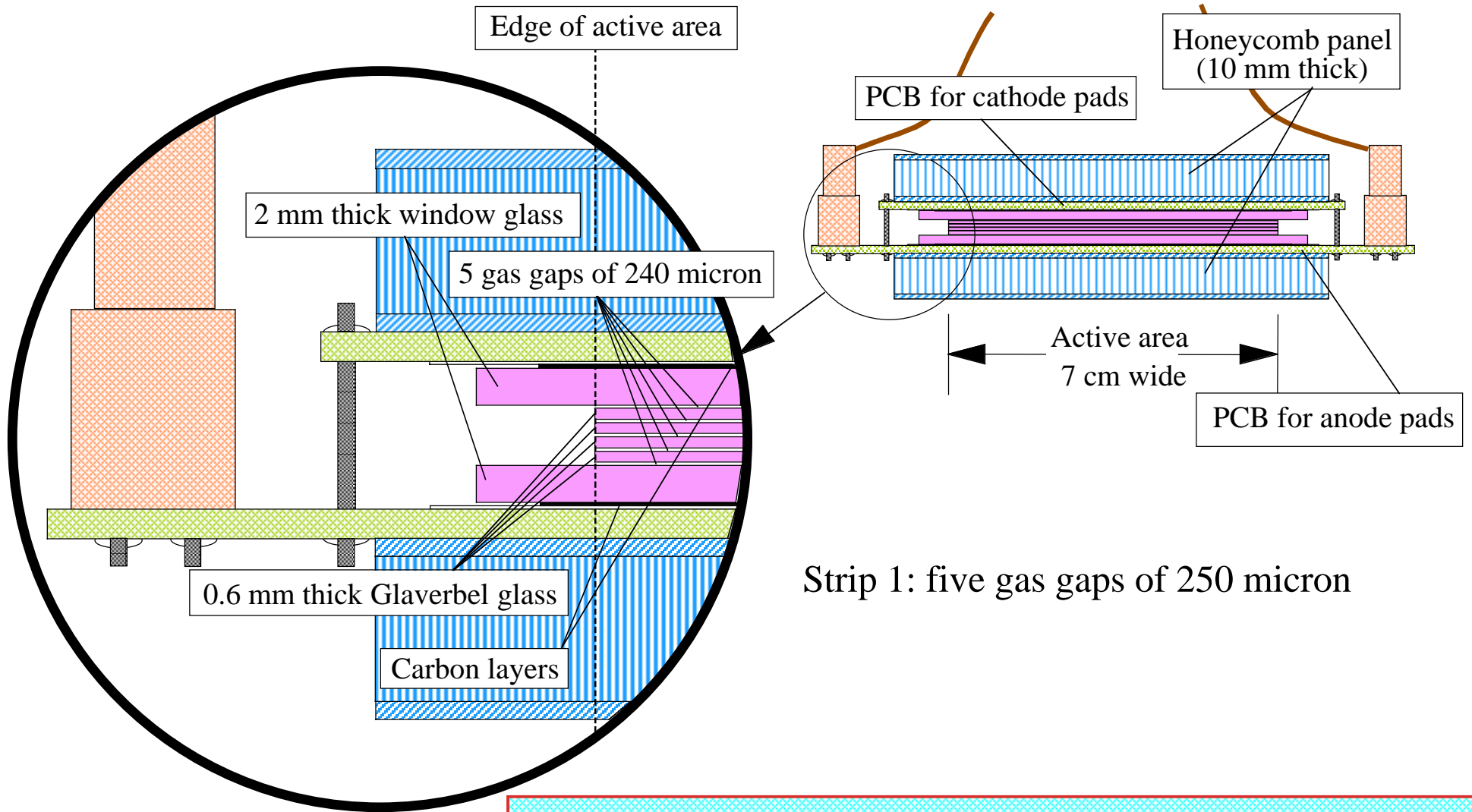
1.2 m length strips

2 x 48 pads

Standard unit detector for ALICE detector  
(ALICE TOF will be constructed with  
~ 16,000 such strips)



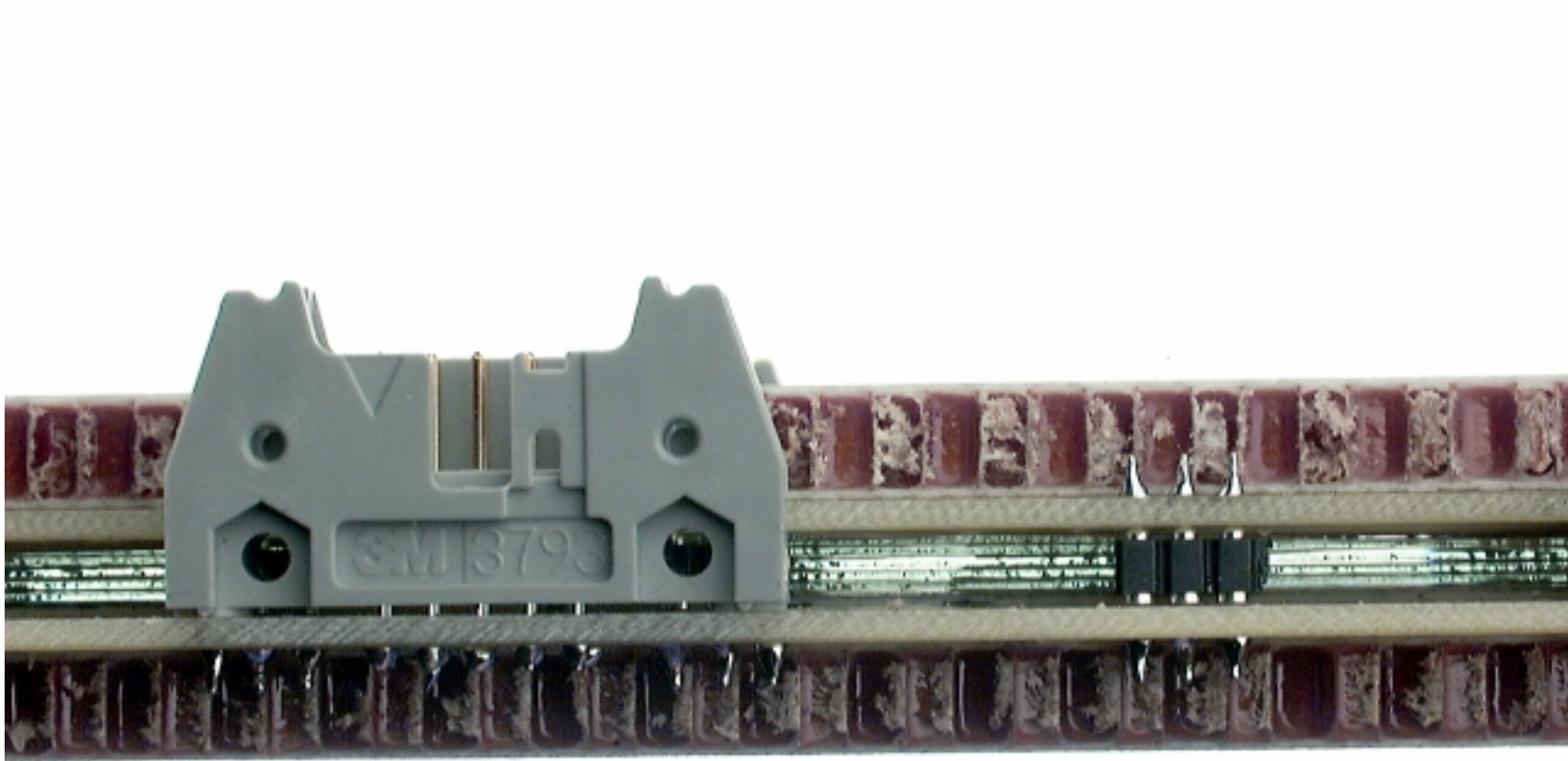




Strip 1: five gas gaps of 250 micron

Spacers: fibre across width of strip every 2.5 cm  
 Edge: defined by edge of cut glass



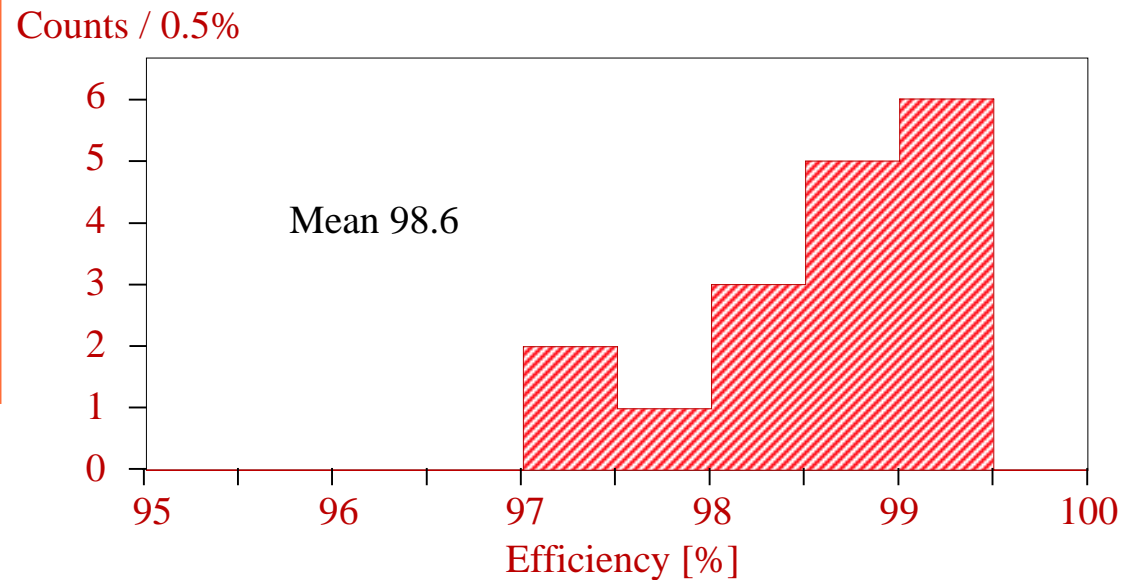
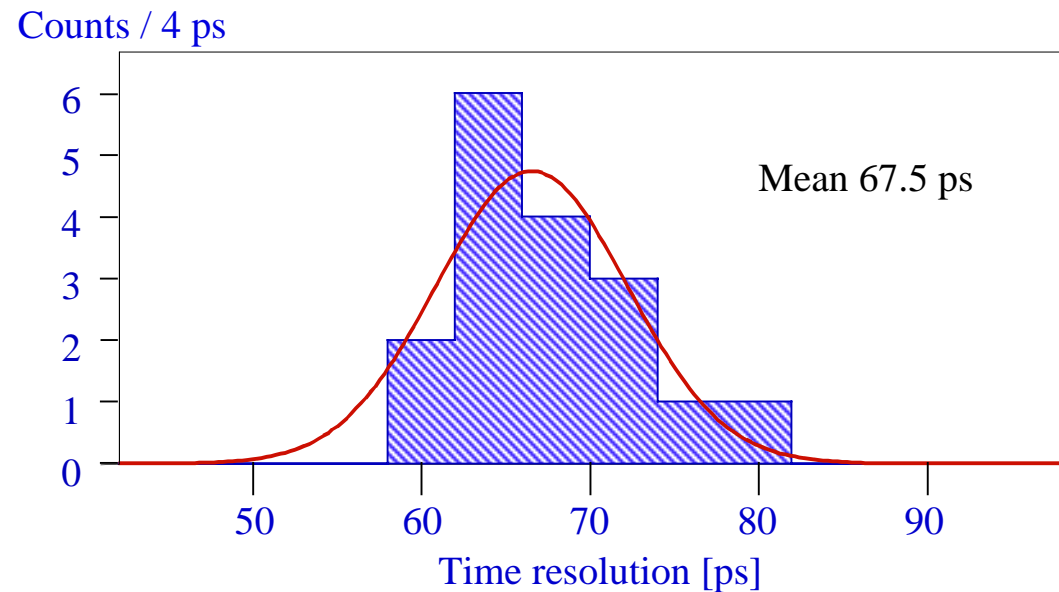


1.2 m length  
ALICE TOF strip

No problem to build long  
strips

Why not?

Question - how precise  
does the gas gap of  $250\text{ }\mu\text{m}$   
need to be?



Question: What happens if the size of the gap is varied??

### STRIP 6

550 micron internal glass sheets  
2.5 mm external glass (Schott black welding glass)  
6 gas gaps of **250 micron**  
fish line spacers across width of strip  
Edge defined by edge of glass  
guard rings



### STRIP 7

550 micron internal glass sheets  
2.5 mm external glass (Schott black welding glass)  
6 gas gaps of **220 micron**  
Fish line spacers across width of strip  
Edge defined by edge of glass  
guard rings

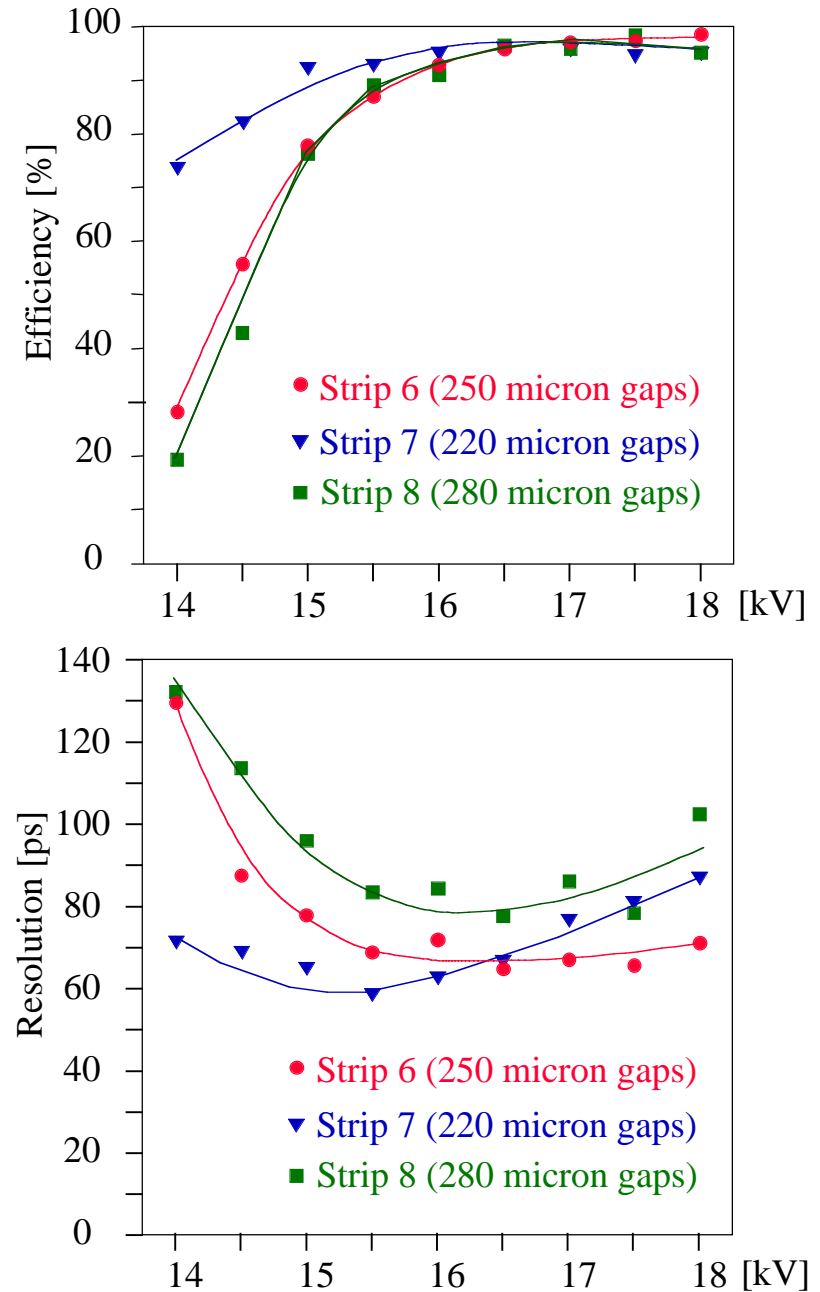
Increase gap by 60 micron  
i.e. **27 %**  
Total gap **1.32 mm**  
increased to **1.68 mm**

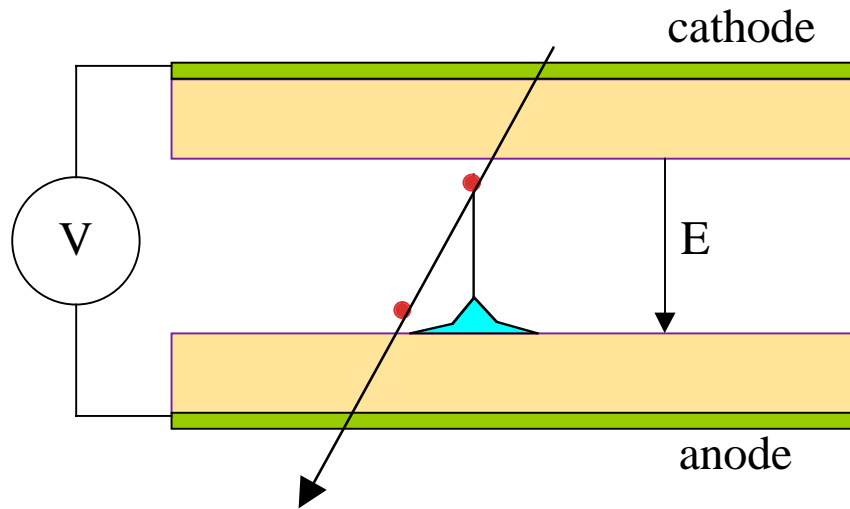
### STRIP 8

550 micron internal glass sheets  
2.5 mm external glass (Schott black welding glass)  
6 gas gaps of **280 micron**  
fish line spacers across width of strip  
Edge defined by edge of glass  
guard rings

Big change in gap size  $\rightarrow$  small change in operating voltage. Large 'plateau' region where efficiency high, time resolution excellent and gap can vary by  $\pm 30 \mu\text{m}$

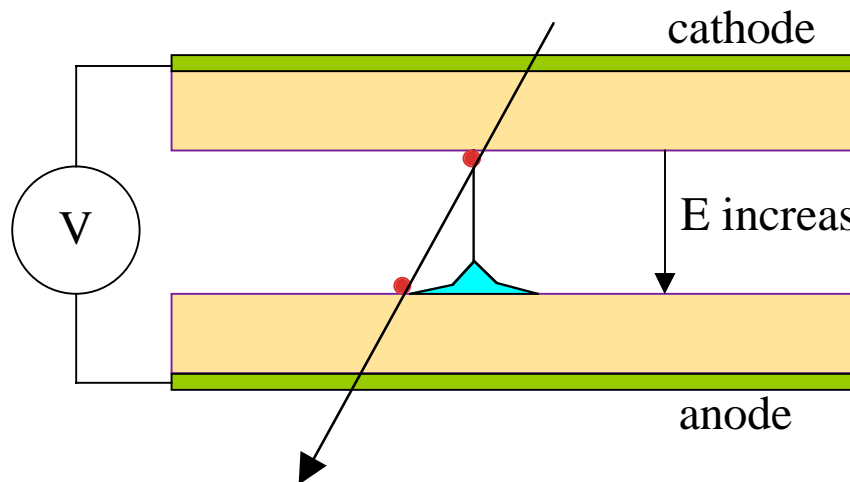
Thus device with this excellent time resolution can be built with very 'relaxed' mechanical tolerances





Charged particle passes through gas gap and creates clusters of electrons and positive ions  
electrons avalanche towards anode → fast signal on external electrodes - etc

Now consider smaller gap



$E$  increased (same  $V$  - smaller gap)

Thus **Townsend coefficient higher** - bigger avalanche  
(i.e. **higher gain**)

however gap smaller therefore **less distance for avalanche to grow**  
(i.e. **lower gain**)

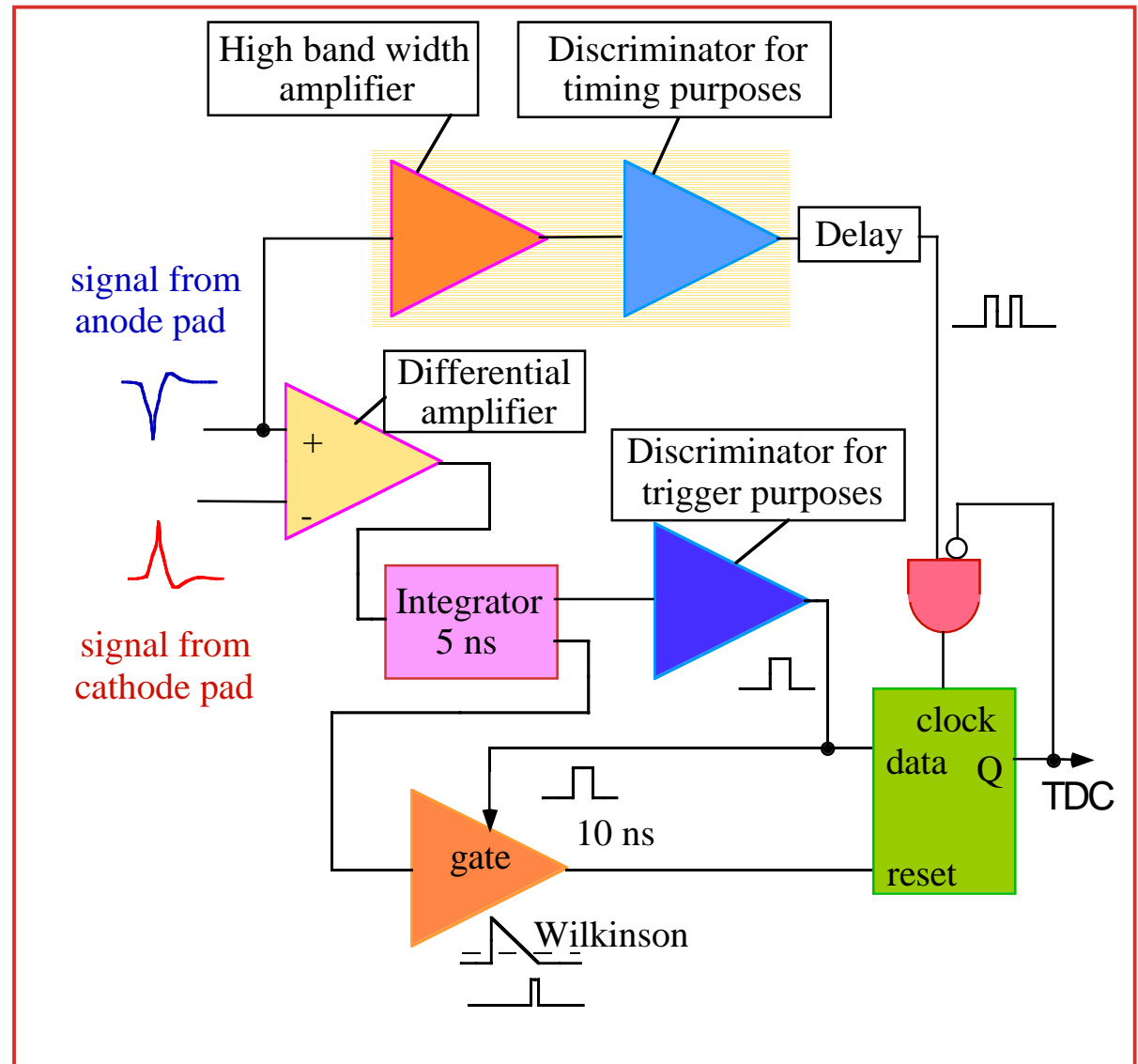
Apparently we are working in region where both effects cancel (by 'magic' it is rather an exact cancellation)



## Proposed electronic scheme presented in TDR

Problem: to get 'best' time resolution need to make timing correction according to pulse height (T(A) corrections).

We need high quality TDC for timing - proposal: convert charge of input signal to Time-over-Threshold and use TDC to measure time of both edges (no ADC required). However need to develop front-end ASIC to keep costs/size/power reasonable.



## 622Mbps, Low-Noise Transimpedance Preamplifier for LAN and WAN Optical Receivers

MAX3760

### General Description

The MAX3760 is a transimpedance preamplifier for 622Mbps ATM applications. It operates from a single +5V supply and typically consumes only 100mW power. The preamplifier converts a small photodiode current to a differential voltage. A DC cancellation circuit provides a true differential output swing over a wide range of input current levels, thus reducing pulse-width distortion.

6.5k $\Omega$  transimpedance gain and 560MHz bandwidth, combined with low 73nA input-referred noise, provide -31.5dBm typical sensitivity in 1300nm receivers. The circuit accepts a 1mA p-p input current, resulting in a typical optical overload of -3dBm. The device operates over an extended temperature range of -40°C to +85°C.

The MAX3760 is internally compensated and requires few external components. In die form it includes a space-saving filter connection, which provides positive bias for the photodiode through a 1k $\Omega$  resistor to VCC. These features, combined with the die aspect ratio and dimensioning, allow the MAX3760 to assemble easily into a TO-style header with a photodiode.

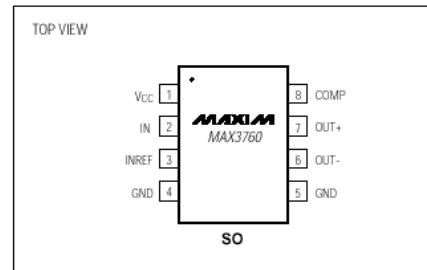
The MAX3760 is designed to be used with either the MAX3761 or the MAX3762 limiting-amplifier ICs. When combined with a photodiode, the chipset forms a complete 5V, 622Mbps receiver. The MAX3760 is available in die form and in an 8-pin SO package.

### Applications

622Mbps ATM LAN Optical Receivers

622Mbps WAN Optical Receivers

### Pin Configuration



### Features

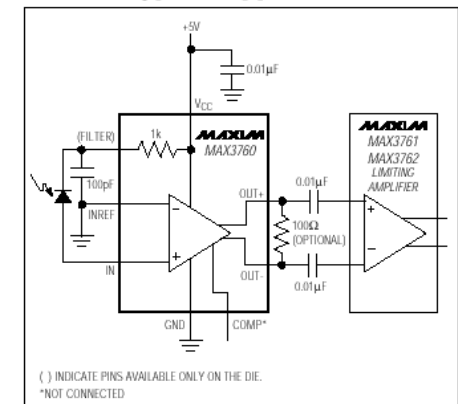
- ♦ 73nA RMS Input-Referred Noise
- ♦ 560MHz Bandwidth
- ♦ 1mA Peak Input Current
- ♦ 6.5k $\Omega$  Gain
- ♦ Operation from -40°C to +85°C
- ♦ 100mW Typical Power Consumption
- ♦ Single +5V Supply

### Ordering Information

PART	TEMP. RANGE	PIN-PACKAGE
MAX3760ESA	-40°C to +85°C	8 SO
MAX3760E/D	-40°C to +85°C	Dice*

\*Dice are designed to operate over a -40°C to +100°C junction temperature ( $T_j$ ) range, but are tested and guaranteed at  $T_A = +25^\circ\text{C}$ .

### Typical Application Circuit



Key point: 560 MHz Bandwidth

Key question: can it be made to work?

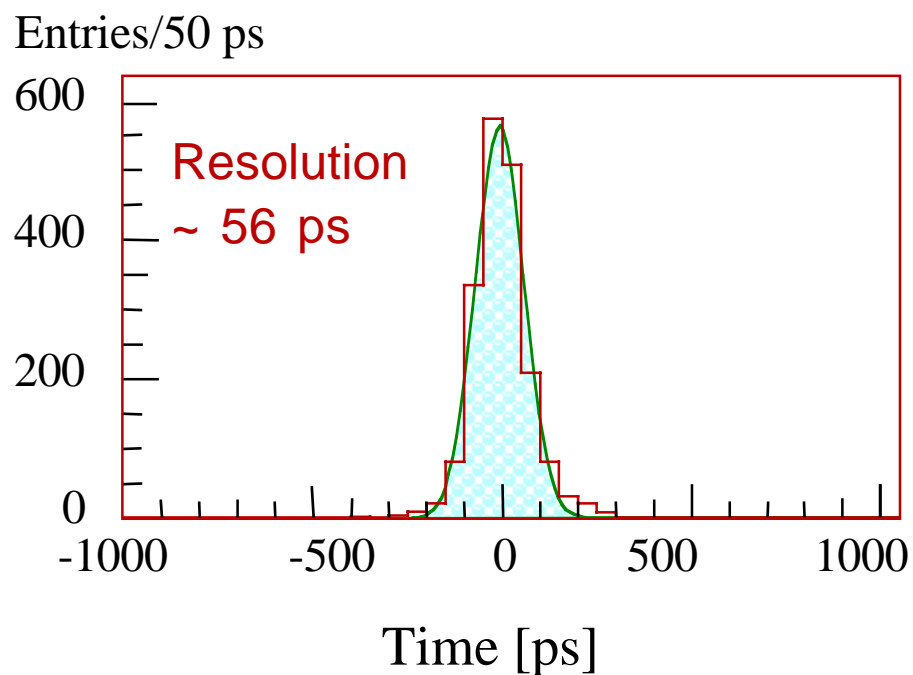
No problem with noise or oscillation (maybe differential output from chamber helps)

MAXIM

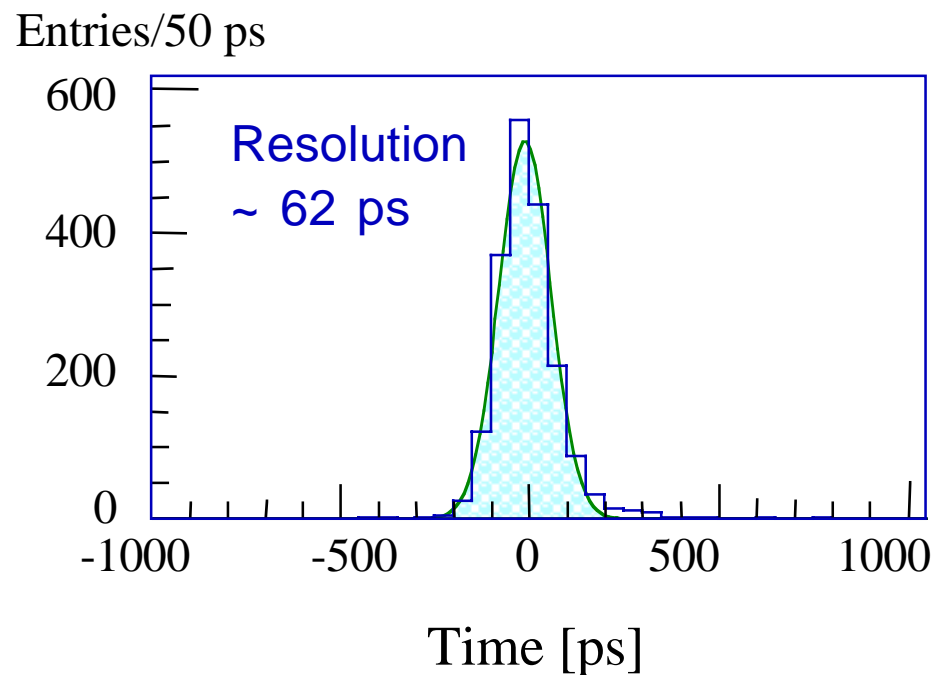
Maxim Integrated Products 1

For free samples & the latest literature: <http://www.maxim-ic.com>, or phone 1-800-998-8800  
For small orders, phone 408-737-7600 ext. 3468.

Using ADC for T(A) corrections



Using Time-over-Threshold for T(A) corrections



## Summary

2 years investigation of multigap resistive plate chamber as a TOF detector

Detector that is easy to build - just make a stack of glass plates

Gap tolerances very relaxed  $\pm 30 \mu\text{m}$  for  $250 \mu\text{m}$  gap

Excellent time resolution  $\sim 70 \text{ ps}$  with insignificant tails  
small “time-walk” ( $\Delta T/\Delta V \sim$  between 0 - 100 ps / 1000V)

Large detectors arrays easy to realise

- (a) differential readout - low noise for electronics
- (b) Loose gap tolerance

Commercial amplifiers ideally suited to detector requirements  
and have reasonable cost (however ASIC  
amplifier-discriminator still under investigation)

**ALICE TOF project is in good shape**